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A Fiber-Optic Voltage Sensor Based on Macrobending Structure

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A fiber-optic voltage sensor based on macrobending structure

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ABSTRACT

We propose and demonstrate an optical voltage sensing scheme based on a macrobending optical fiber in a ratiometric power measurement system. This novel approach to sensing has not been utilized before and has the advantage that the sensor involves simple fabrication compared to existing fiber-optic voltage sensors. To prove the feasibility of such a fiber-optic sensor, a sensor for a voltage range from 0∼100 V is demonstrated, with a resolution of 0.5 V. The sensor is robust, linear, and shows a competitive measurement resolution. The sensor can be easily scaled to suit other voltage levels and be effectively combined with optical current sensors.

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1. Introduction

Fiber-optic voltage sensors are attractive for high voltage sensing applications as they can provide high dielectric isolation between the high voltage measurement point and the measurement electronics. Such sensors also offer many other advantages compared with conventional voltage sensors such as immunity to electromagnetic interference, light weight, small size, fast response, and a potential for remote operation [1]. Piezoelectric (PZT) devices are often implemented as transducers in fiber-optic voltage sensors. The voltage induces a strain in the PZT as well as in the optical fiber attached to it. The attached optical fiber could be of any type such as a singlemode fiber [2], a hollow fiber [3], or a fiber Bragg grating (FBG) [4]. Depending on the type of the fiber sensor employed the measurement of voltage can be carried out either using the interference between the reflected and incident signal measurement [2,3] or by measuring the reflected signal shifts [4] However these existing schemes require complex and expensive measurement systems to extract either the phase information or the wavelength information in order to measure the voltage. We have previously presented a singlemode–multimode–singlemode (SMS) structure based fiber-optic voltage sensor that utilized a ratiometric power measurement system [5]. In this paper a strong voltage dependence for the transmission loss of the SMS fiber structure can be achieved at a single wavelength facilitating the use of an inexpensive interrogation system. However, the accurate fabrication of an SMS sensing structure still needs a relatively complex fabrication process.

Recently a macrobending fiber structure has been demonstrated for various applications such as: edge filter for the fast wavelength measurement [6], temperature sensor [7], refractive index sensor [8], textile based respiratory rate sensor [9], flowmeter [10], and biosensor [11]. In this paper we present for the first time a simple method to measure voltage using a macrobending fiber attached to a PZT stack utilized in a ratiometric power measurement scheme. A DC voltage sensor is demonstrated for a range of voltages from 0 to 100 V, which is suitable for isolated voltage monitoring, for example, in solar power systems or in automotive and aircraft electrical systems. The proposed sensor has the potential to be applied in high voltage sensing applications.

2. Fiber sensing background and operating principle

In our previous work [6], a bare 1060XP fiber coated with an absorbing layer has been proposed as an edge filter for wavelength measurement applications. Both theoretical and experimental results have shown that the bend loss monotonically decreases as the bend diameter increases at certain specific wavelengths. Such a characteristic offers a possibility to develop a macrobending-based displacement sensor. The operating principle of such a sensor is based on the fact that a change in the bend diameter of the fiber section causes a change in the bending loss. By measuring the changes in macrobending loss, the variation in bend diameter can be determined and with a suitable calibration the displacement can be measured.

It should be noted that using the bare 1060XP fiber coated with an absorbing layer as the basis for a displacement sensor would result in a low resolution for the proposed sensor. From

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Ref. [12], which also utilizes a 1060XP fiber, one can see that the measured discrimination range (bend loss difference between the bend radius of 8.5 and 14 mm) is 15.5 dB at an operating wavelength of 1500 nm, which yields an estimated resolution for displacement measurement of 0.0014 dB/μm. Given that optical power measurement normally cannot achieve a resolution better than 0.02 dB, the result is that micron order displacement sensing cannot be achieved using this fiber configuration. Furthermore, the limitations of the absorbing layer applied to the fiber surface, evident from the quasi-periodic nature of the measured results, can further degrade the accuracy of displacement measurement.

One possible solution to increase the sensitivity of the proposed macrobending fiber sensor is to utilize the inherent Whispering Gallery Mode (WGM) effect in a fiber bend. Refs. [13,14] have investigated this approach using a bare bending SMF28 fiber, where strong WGMs significantly affect the light propagation through the bending fiber. The measured bend loss results show a large discrimination range (~7.3 dB) between the bend radii of 6 and 5.5 mm, at a wavelength of 1600 nm [13]. Such a performance indicates that WGMs could be potentially useful to enhance the sensitivity of a displacement sensor based on a macrobending fiber loop. However because of the low value of bend loss in SMF28, a displacement sensor using SMF28 would require many fiber turns to achieve a reasonable resolution, which in practice would create significant mechanical difficulties for the sensor.

The alternative approach is to use a high bend loss fiber, allowing the sensor to be fabricated with only a half-loop of fiber. In this paper, the proposed fiber displacement sensor consists of a half-loop structure of coating stripped bare high bend loss fiber. The fiber employed in the experiment was a 1060XP singlemode fiber that has a high bend loss over the wavelength range of 1500–1600 nm. Experimentally to fix the diameter of the fiber half-loop, each end of the half-loop is glued to a 20 mm travel single-axis translation stage, which can achieve a 10 μm step resolution. In this way the diameter of the bend fiber can be controlled using the translation stages.

We measured the bend loss of a bare 1060XP fiber with a cladding diameter of 125 μm using a tunable laser and an optical spectrum analyzer, for the range of bend diameters from 15 to 18 mm (the bend length is half turn) in the wavelength range from 1500 to 1600 nm. The bending loss responses in the wavelength range 1500–1600 nm for different positions of the translation stage are presented in Fig. 1 for bend diameters of circa 17 mm.

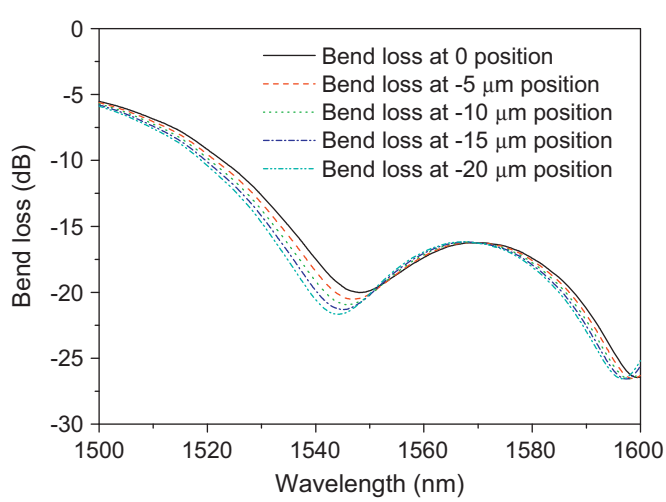

Fig. 1. Bend loss response of a bare bend fiber with a half-loop.

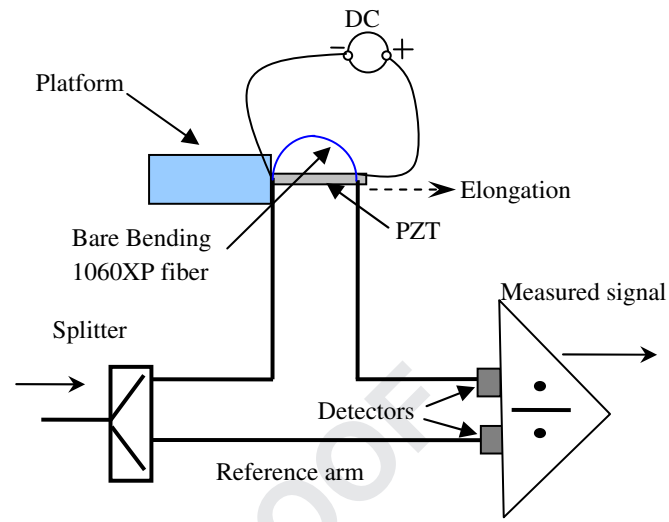

Fig. 2. Schematic configuration of the proposed bent fiber voltage sensor system.

It is evident from Fig. 1 that for a given bend diameter there is a complex relationship between the transmitted wavelength and bend loss, which arises because of WGMs. At specific wavelengths the presence of WGMs means that the bending loss is a very strong function of the bend diameter. For example, for a wavelength of 1540 nm, one can see that the difference in bend loss between 16.98 and 17 mm is circa 3.07 dB, which could provide a useful displacement resolution. Note that it is found that beyond the 18 mm bend diameter the intensity of WGMs is too low to provide a useful sensitivity enhancement, while for bend diameters below 15 mm, the risk of fiber breakage by excessive stress is too high.

The voltage sensor can be built by attaching the half-loop fiber displacement sensor to a PZT stack, as shown in Fig. 2. One end of the PZT stack is bonded to a fixed platform and the other end to a light weight T-shaped base. Two points of the half-loop of the bend fiber are also glued to the platform and the base. The displacement produced by the PZT, when voltage is applied, changes the distance between the fixed points of the fiber and therefore changes the bend diameter. As it is shown in Fig. 1 above, a decrease in the bend diameter causes the peak of the spectral response to shift toward a lower wavelength. It is found that at some fixed operating wavelength and within some range of bend diameters corresponding to the range of voltages applied to the PZT the transmission loss of the bend fiber changes monotonically with the bend diameter. Thus, the transmission loss of the bend fiber will vary in proportion to the applied voltage.

Fig. 2 shows a schematic configuration of the voltage sensor in the ratiometric scheme. The voltage information is extracted using a ratiometric power measurement system. The measured ratio is independent on the input signal power variation that provides more stable and accurate measurements. The input signal is divided into two equal power signals, one of which goes to the reference arm and the other goes to the bend fiber. Two photodiodes and the associated electronics are used to measure the output power from the two arms. The unknown voltage can be found by measuring the power ratio of the two output photodiodes, assuming that the system is calibrated.

3. Experimental results and discussion

A commercial PZT stack AE0505D18 (manufactured by Tokin Corporation, Japan) was used as the transducer. It has a length of

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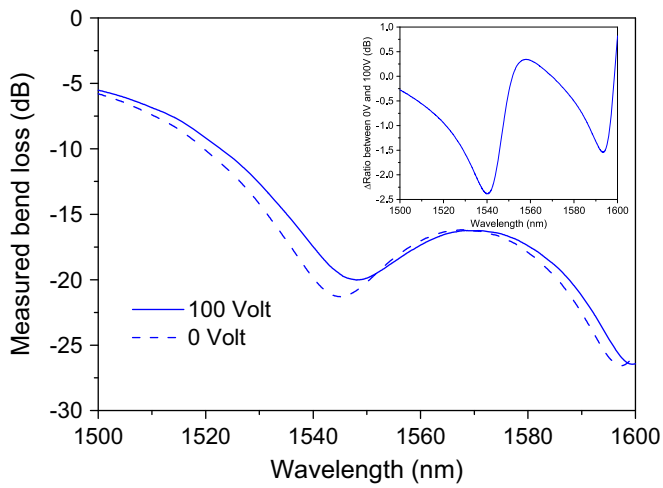

Fig. 3. Measured ratio spectral responses at 100 and 0 V (inset: ratio difference).

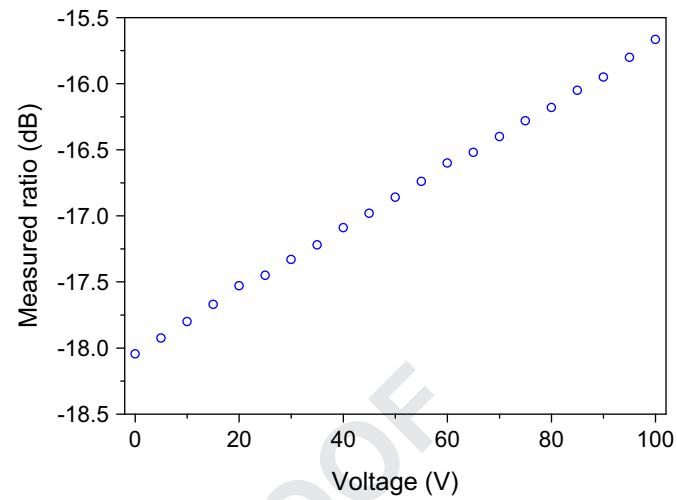

Fig. 4. Measured ratio response of the sensor against voltage (0~100 V) at the operating wavelength of 1540 nm (variation in ratio for a step change of 750 nm (corresponds to a 5 V voltage step applied to the PZT)).

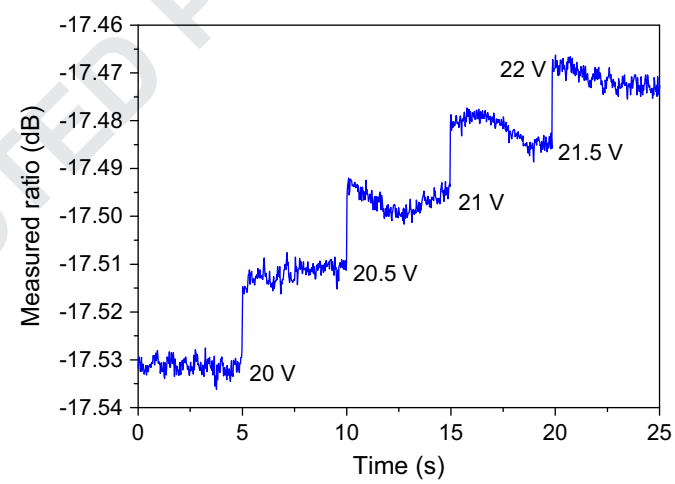

Fig. 5. Measured output ratio response of the sensor versus time (0~25 s) at the operating wavelength of 1540 nm (variation in ratio for a step voltage change of 0.5 V).

20 mm, cross section dimensions of 5 × 5 mm and can produce the maximum elongation of 15 μm at a DC voltage of 100 V. The bare high bend loss fiber 1060XP was used for the voltage sensor head. The bend diameter of the fiber was in the range from 15 to 18 mm resulting in a single-peak spectral response over the wavelength range of 1500–1600 nm [13]. As shown in Fig. 2 the bare bend fiber is glued to the platform and the base, with a total length in between the fixed points of about 17 mm.

A tunable laser TUNICS-PLUS was used as the input signal source. A single channel piezo controller MDT694A (Thorlabs) was used to supply the DC voltage from 0 to 100 V to the PZT stack. Initially two spectral responses of the output ratio were measured at voltages 0 and 100 V to select the appropriate operating wavelength. The measured spectral ratio responses at 0 and 100 V in the wavelength range of 1500–1600 nm with an increment of 0.1 nm are shown in Fig. 3. It can be seen that the spectral ratio response of a bare bent fiber is shifted to a lower wavelength when the voltage is applied. This spectral response shift to the lower wavelength region confirms the strain effect on the bare bent fiber as in Ref. [15].

For the purpose of power based measurement, it is necessary to select an optimal fixed operating wavelength for the ratiometric system. The difference in the measured ratio at 100 and 0 V versus wavelength is presented in the inset of Fig. 3. From the figure, one can see that a stronger voltage dependence is obtained at some wavelengths, which is more suitable as the operating wavelengths for the proposed voltage sensor. A wavelength of 1540 nm with a highest ratio difference of −2.379 dB is selected as an operational wavelength in the following experimental investigation.

The measured ratio response versus voltage applied to the PZT from 0 to 100 V with an increment of 5 V at the wavelength of 1540 nm, is presented in Fig. 4. A linear relation between the applied voltage and the ratio response is demonstrated with a slope of 0.0238 dB/V. To estimate the voltage measurement resolution of the system, step changes of 0.5 V from 20 to 22 V are applied to the fiber sensor with time intervals of 5 s. The measured ratio variations versus time are shown in Fig. 5. It is clear that the resolution of the voltage sensing system is better than 0.5 V. Thus it is demonstrated that the proposed fiber sensor with macrobending fiber structure, together with a PZT is suitable for DC voltage measurements in the range of voltages from 0 to 100 V.

It is possible to extend the voltage range for the bent fiber sensor to higher voltages. The operating voltage depends on the PZT's strain–voltage characteristic. In Ref. [4], a PZT is used that can be operated over a much higher AC voltage range from 0 to 5 kV with a maximum PZT displacement of about 19 μm, which is similar to the maximum PZT displacement used in this paper. The maximum PZT displacement should be within the limits of the measureable displacement range of the bent fiber, which is approximately 250 μm in the present case.

4. Conclusions

A macrobending fiber structure attached to a PZT transducer is proposed as a voltage sensor employed in a ratiometric power measurement scheme. A DC voltage sensor in the voltage range from 0 to 100 V with a resolution of about 0.5 V is demonstrated. The proposed fiber sensor has a low cost, fast measurement capability, and a potential for high voltage measurement applications.

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